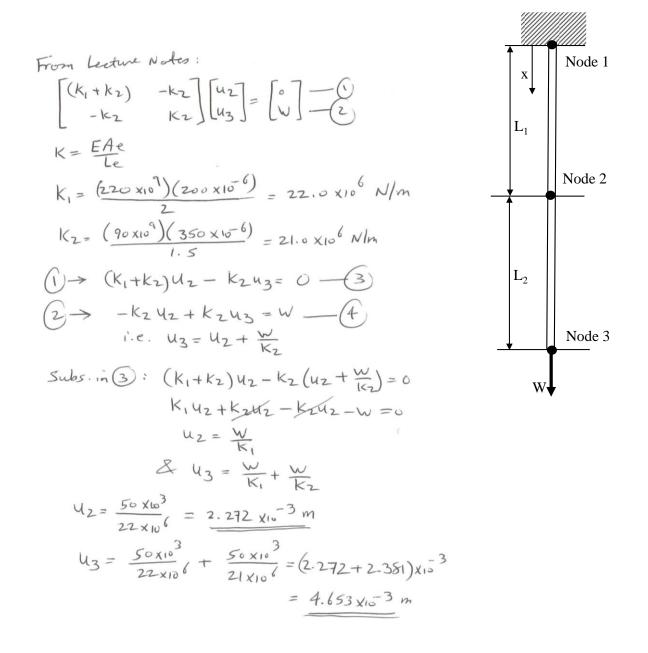
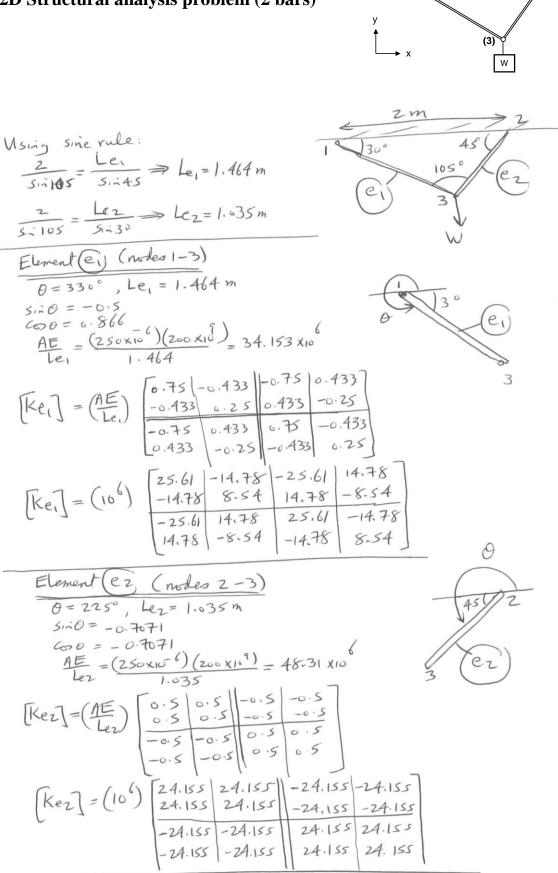
SOLUTIONS Exercise Sheet (FE)-1 (Pin-Jointed Elements)

1.1D pin-jointed problem



2. 2D Structural analysis problem (2 bars)

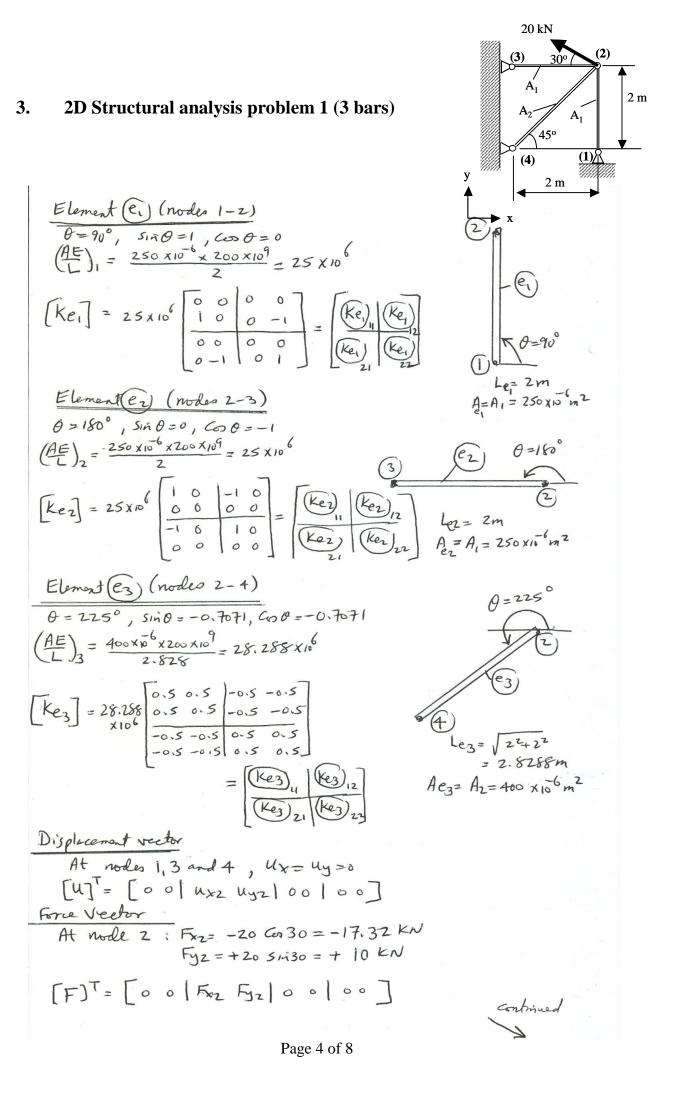


2 m

(2)

450

30°



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(4) 2 m 50 kN (2) 300 2D Structural analysis problem 2 (3 bars) 4. 2 m (3)2 m $\frac{\text{Elenert}(e_1): \text{Nodes } 1-2}{\theta=0^\circ, \text{ Cor } \theta=1, \text{ sin } \theta=0}$ (T) $\frac{AE}{Le_{1}} = \frac{200 \times 10^{-6} \times 200 \times 10^{9}}{2}$ $k_{e_1} = AE \begin{bmatrix} 1 & 0 & | -1 & 0 \\ 0 & 0 & 0 & 0 \\ \hline e_r & | -1 & 0 & | & 1 & 0 \\ \hline -1 & 0 & | & 1 & 0 \end{bmatrix}$ = 20 ×106 00 (Key (kei) II $k_{e_1} = (0^6)$ Keiln Kei Elevent(ez): Notes 2-3 0=270°, Co0=0, Sii0=-1 (2 ez 0000 Kez = AE Lez AE 200 X10 6 X200 X10 1 0 1 0 20 0 -20 = 20 x10 (Keziz $k_{e_2}=(10^6)$ Element(C3): Noder 2-4 $\theta = 45^{\circ}, C_{0} \theta = 0.707, Si \theta = 0.707 = 1/2$ $K_{e3} = AE \begin{bmatrix} 0.5 & 0.5 & -0.5 & -0.5 \\ 0.5 & 0.5 & -0.5 & -0.5 \\ -0.5 & -0.5 & 0.5 & 0.5 \\ -0.5 & -0.5 & 0.5 & 0.5 \\ -0.5 & -0.5 & 0.5 & 0.5 \end{bmatrix}$ 150 X10 6 x 200 X107 V8 (AE Les 10.607 x10 $K_{e_3} = \begin{pmatrix} 10^6 \end{pmatrix} \begin{bmatrix} 5.303 & 5.303 & -5.307 & -5.363 \\ 5.303 & 5.363 & -5.363 & -5.363 \end{bmatrix}$ -5.303 -5.303 5.303 5.303 -5303 -5.313 5.3.3 5.3.3 Displacement vector <u>At nodes 1, 3, 4</u>: 4x=4y=0 [4]^T = [00 | 4x2 4y2 | 00 | 00] Force Vector At Node 2: Fx= -50630 = -43.30 KN Fy=+505+130 = +25.0 KN [F]T=[00|Fx2 Fy2|00|00]

Page 6 of 8

Matrix Assently 0 (Ke VII (Kei)12 0 0 0 0 0 122 Ker) Froz Ux7 Kei) Ke3)12 442 fy2 (e3)4 = 0 0 Kez) Kez/21 O 0 0 0 D 0 Kez ()Kez 0 6 -20 0 20 0 0 0 0 0 0 0 0 -43.3 +25.0 (103) (20+0+5.303) (0+0+5.303) uzz 00 -5.3 -5.7 20 0 2 (10 (0+0+5.303) (0+20+5.303) 0 -20 OO -5.3 -5. Myz 0 C 0 0 0 U 0 0 - 20 0 20 0 0 0 0 5.3 5.3 -5.303 - 5.303 Ó 0 5.3 53 -5.303 -5.3.3 The system of equations can be reduced to two equations only C $z_{5,303}$ $g_{,3,3}$ u_{xz} = $\begin{bmatrix} -43,3\\25,0 \end{bmatrix}$ x_{10}^{-3} 5,303 $z_{5,303}$ u_{yz} = $\begin{bmatrix} -43,3\\25,0 \end{bmatrix}$ x_{10}^{-3} (25.303) $u_{x2} + (5.303)$ $u_{y2} = 43.3 \times 10^{-3} - -(1)$ (5.303) $u_{x2} + (25.303)$ $u_{y2} = + 0.00 \times 10^{-3} - -(2)$ From (): Ux2=- 1.711 x10-3- (0.2095) Uy2 -3 Subs. in (2): (5.303) $\left[-1.711 - x10^3 - (0.2095) uy_2 \right] + 25.313 uy_2 = 25 x10^3$ (24.192) $uy_2 = +34.073 x 10^3$ 4yz=+1.408×10-3 m Ux7 = -2.006×10-3 m 1 Strees in clement 2-4
$$\begin{split} & (\delta_{e}] = \underbrace{E}_{Le} \left[\begin{array}{c} -\omega \sigma & -s_{n} \sigma & \sigma \sigma & s_{n} \sigma \end{array} \right] \underbrace{ \begin{bmatrix} u_{x} \\ u_{y} \\ u$$
29.89 x 10⁶ Pa (tensile)

5. Torsional Element

This question demonstrates that the principle of minimum TPE can be applied to other physical problems. Here the variables on the torsional element are the angle (θ) and the torque (T), whereas in the lecture notes we used "displacement" and "force" as the variables. The same derivation steps based on the principle of minimum TPE can also be used in the torsional element.

(a) Mini. Tohal Potential Energy:
Given: T.P.E. =
$$\int_{0}^{1} \frac{GJ}{2} \left(\frac{d\rho}{dx}\right)^{2} dx - T_{i}\theta_{i} - T_{2}\theta_{2}$$

Assuming a linear variation of 0 along the length L:
 $\theta = c_{1}x + c_{2}$
at $x = 0$, $\theta = \theta_{1} \implies \theta_{1} = C_{1}(0) + c_{2} \implies C_{2} = \theta_{1}$
 $dt x = L$, $\theta = \theta_{1} \implies \theta_{2} = c_{1}(L) + \theta_{1} \implies C_{1} = \frac{\theta_{2} - \theta_{1}}{L}$
 $\frac{d\theta}{dx} = c_{1} = \frac{\theta_{2} - \theta_{1}}{L}$
Subs. in T.P.E. $\implies TPE = \int \frac{GJ}{GJ} \left(\frac{\theta_{2} - \theta_{1}}{L}\right)^{2} dx - T_{i}\theta_{1} - T_{2}\theta_{2}$
 $TPE = \frac{GJ}{GJ} \left(\frac{\theta_{2} - \theta_{1}}{L^{2}}xL - T_{i}\theta_{i} - T_{2}\theta_{2}$
 σ_{1} , in matrix form: $TPE = \left(\frac{1}{2} \frac{GJ}{2}\right)\left[\theta_{i} \theta_{2}\right] - T_{i}\theta_{i} - T_{2}\theta_{2}$
 $\theta_{1} = 0 = \frac{1}{2} \frac{GJ}{GJ} \left(0x^{2} - 2\theta_{i}\theta_{2} + \theta_{1}^{2}\right) - T_{i}\theta_{1} - T_{2}\theta_{2}$
 $\frac{\delta TPE}{\partial \theta_{1}} = 0 = \frac{1}{2} \frac{GJ}{GJ} \left(-2\theta_{2} + 2\theta_{1}\right) - T_{i} - 0$
 $\frac{\delta TPE}{\partial \theta_{1}} = 0 = \frac{1}{2} \frac{GJ}{GJ} \left(-2\theta_{2} + 2\theta_{1}\right) - T_{i} - 0$
 $\frac{\delta TPE}{\partial \theta_{2}} = 0 = \frac{1}{2} \frac{GJ}{GJ} \left(2\theta_{2} - 2\theta_{1}\right) - 0 - T_{2}$
 $\frac{\delta TTE}{\partial \theta_{2}} = 0 = \frac{1}{2} \frac{GJ}{GJ} \left(2\theta_{2} - 2\theta_{1}\right) - 0 - T_{2}$
 $\frac{\delta TTE}{\partial \theta_{2}} = 0 = \frac{1}{2} \frac{GJ}{GJ} \left(2\theta_{2} - 2\theta_{1}\right) - 0 - T_{2}$
 $\frac{\delta TTE}{\partial \theta_{2}} = 0 = \frac{1}{2} \frac{GJ}{GJ} \left(2\theta_{2} - 2\theta_{1}\right) - 0 - T_{2}$
 $\frac{\delta TTE}{\partial \theta_{2}} = 0 = \frac{1}{2} \frac{GJ}{GJ} \left(2\theta_{2} - 2\theta_{1}\right) - 0 - T_{2}$
 $\frac{\delta TTE}{T} = \frac{GG}{G} \implies T = GJ \left(\frac{\theta_{2}}{T}\right)$
In matrix form : $\left[\frac{T_{1}}{T_{2}}\right] = \left(\frac{GJ}{C}\right) \left[\frac{1}{-1} - 1\right] \left[\frac{\theta_{1}}{\theta_{2}}\right]$
Hence $T_{1} = \frac{GJ}{G} \left(\theta_{1} - \theta_{2}\right)$
 $T_{2} = \frac{GJ}{G} \left(\theta_{2} - \theta_{1}\right)$
 $\sigma = \left[\frac{T_{1}}{T_{2}}\right] = \left(\frac{GJ}{L}\right) \left[\frac{1}{-1} - 1\right] \left[\frac{\theta_{1}}{\theta_{2}}\right] - \cdots \alpha_{0}(\alpha)$